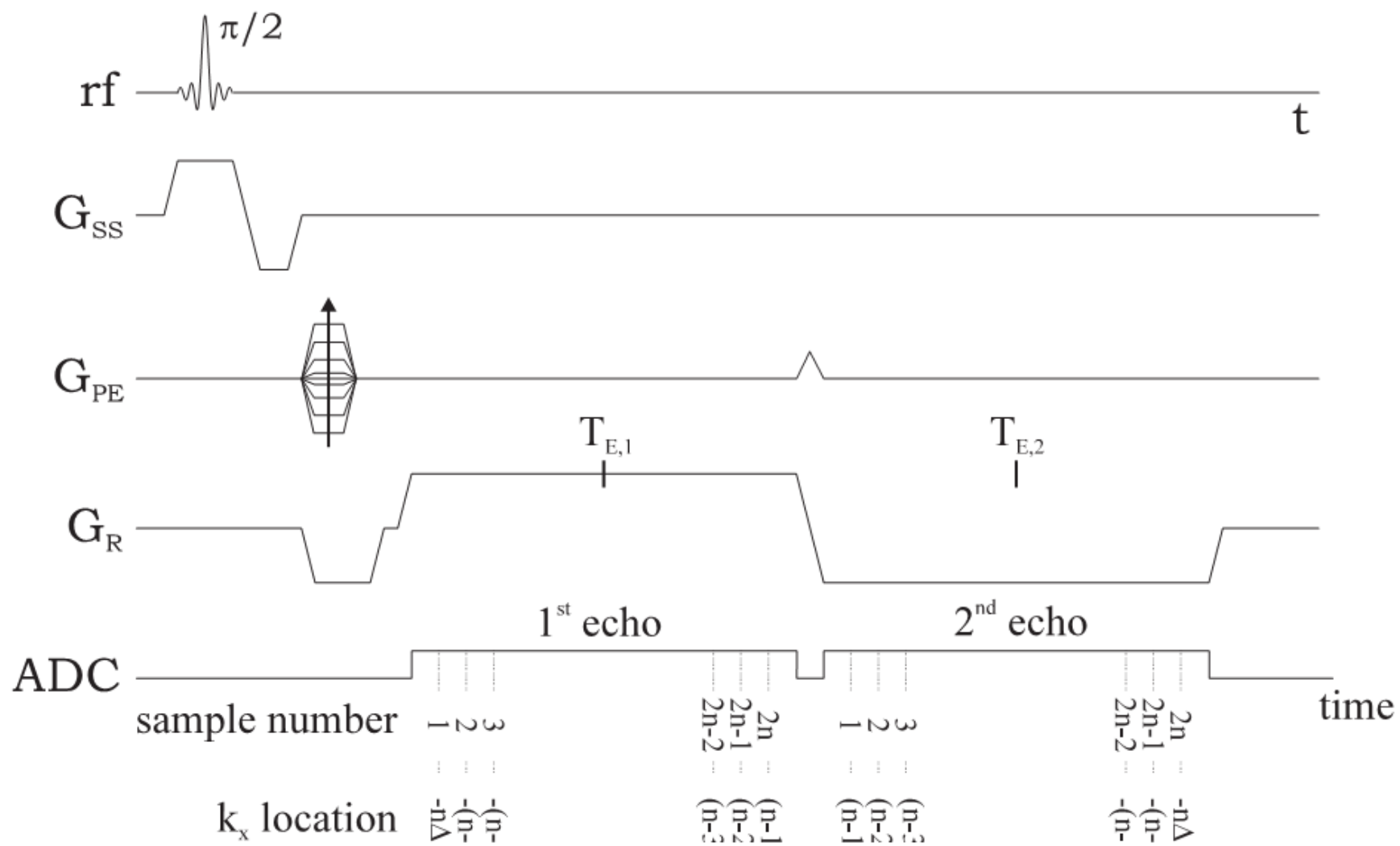
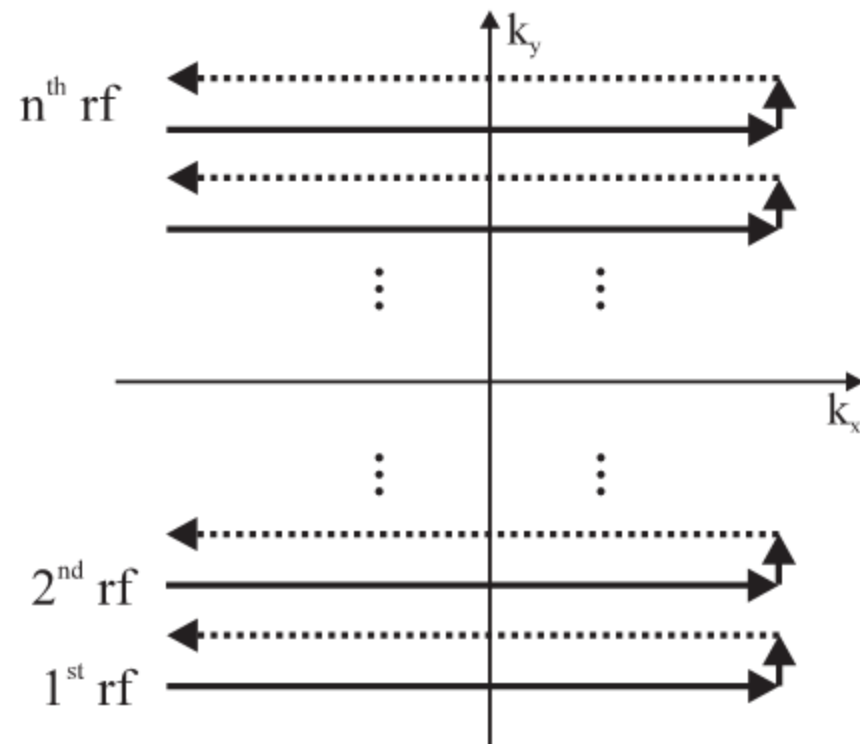
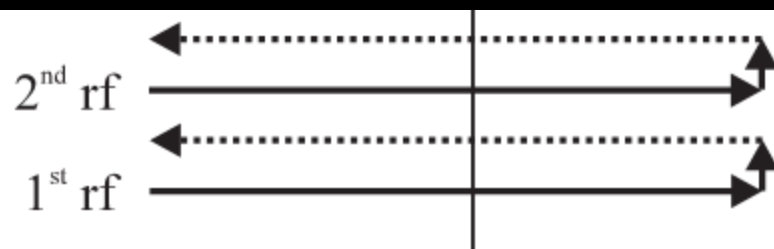
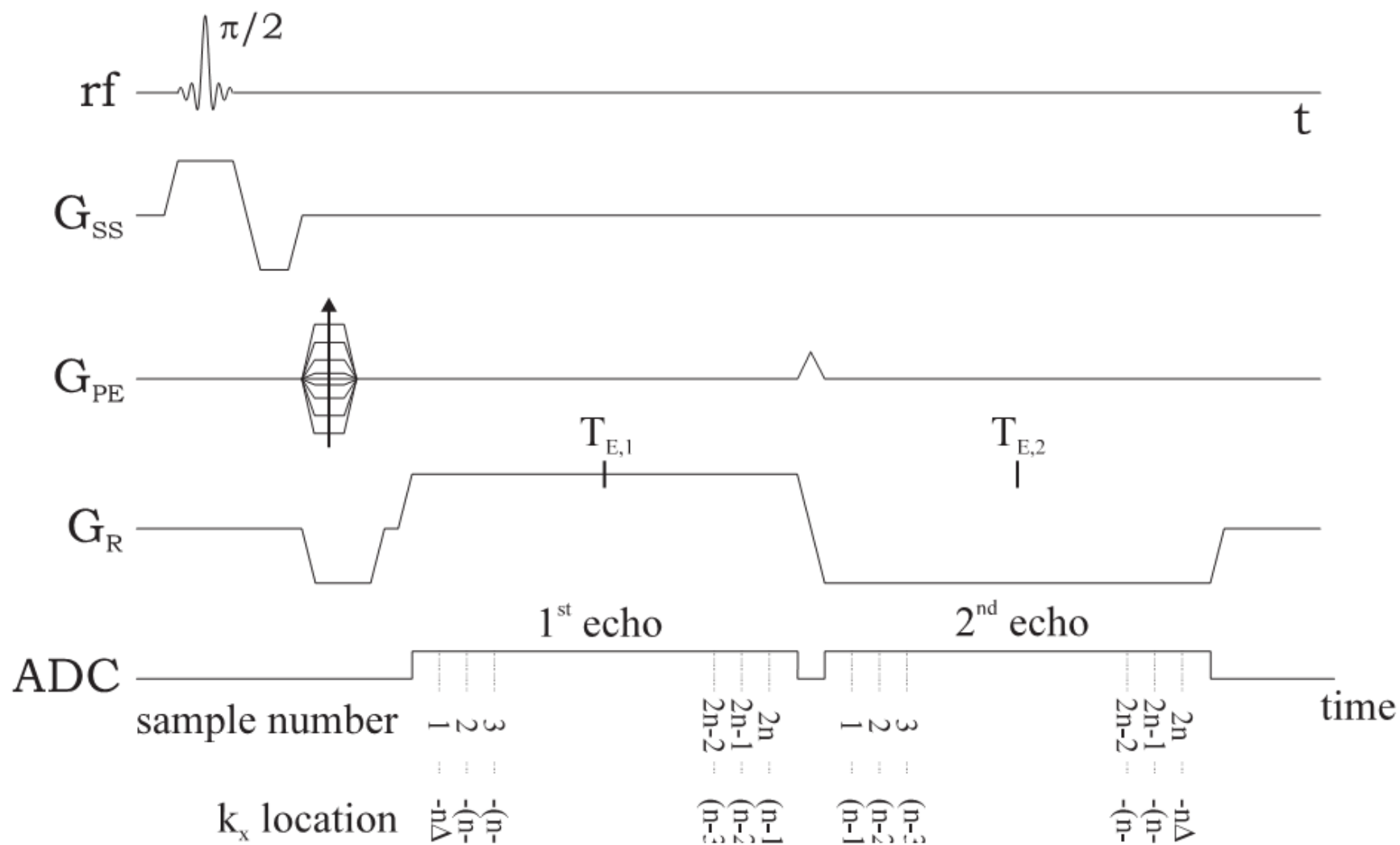


Chapter 19 and 22



segmented k -space image (double echo example)





Even Lines

$$u_{first\ echo}(k_x, k_y) =$$

$$\Delta k_x \Delta k_y \sum_{r=-n}^{n-1} \sum_{p=-n/2}^{n/2-1} e^{-T_{E,1}/T_2^*} e^{-r\Delta t/T_2^*} \delta(k_x - r\Delta k_x) \delta(k_y - 2p\Delta k_y)$$

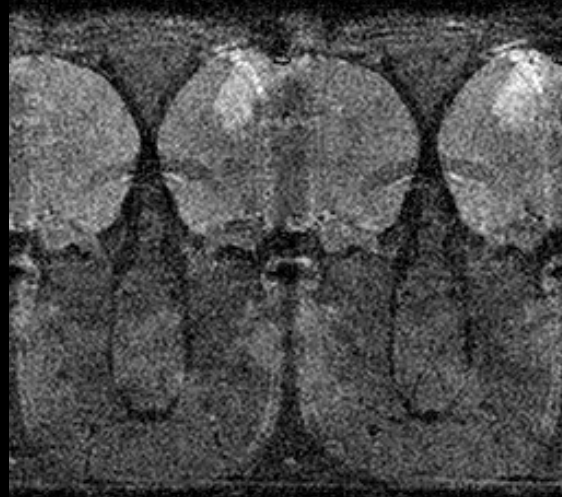

Odd Lines

$$u_{second\ echo}(k_x, k_y) =$$

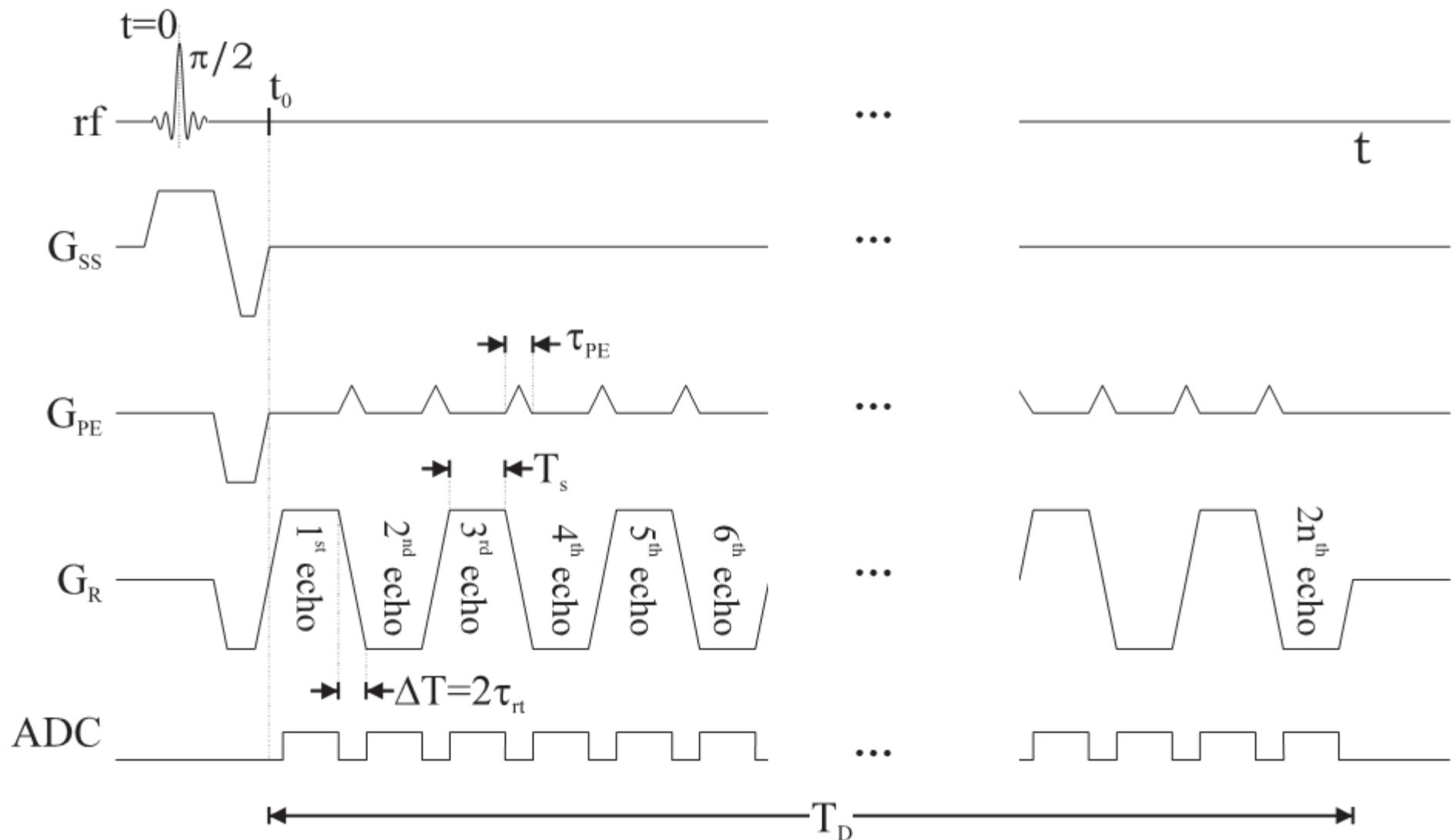
$$\Delta k_x \Delta k_y \sum_{r=-n}^{n-1} \sum_{p=-n/2}^{n/2-1} e^{-T_{E,2}/T_2^*} e^{+r\Delta t/T_2^*} \delta(k_x - r\Delta k_x) \delta(k_y - (2p+1)\Delta k_y)$$


Combined Sampling Function

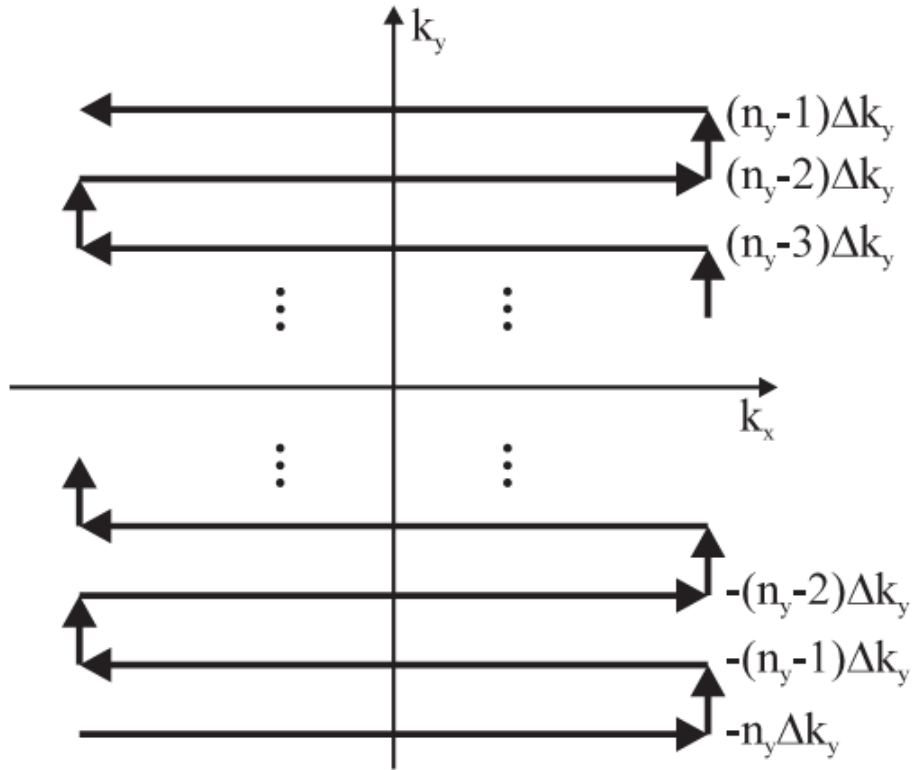
$$u(k_x, k_y) = u_{first\ echo}(k_x, k_y) + u_{second\ echo}(k_x, k_y)$$



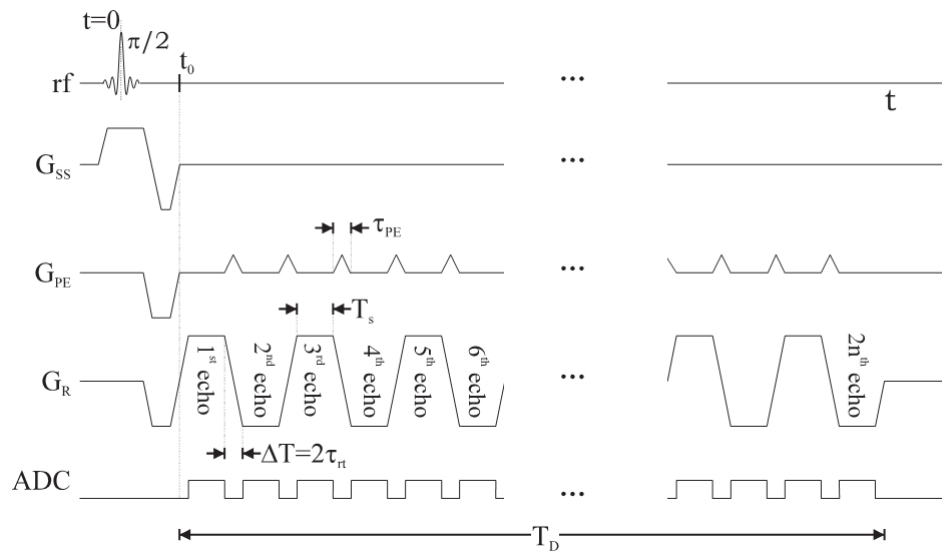
EPI sequence with rectilinear sampling and sequential coverage of k-space



TE
TR
Lx
Ly
 Δx
 Δy



Time at which the central part of the k-space is sampled is the echo time



TD – Total time for which the read out gradient is played out

T_s – total sampling time for an echo

ΔT – peak-to-peak gradient ramp time

τ_{rt} – gradient ramp time from zero to peak

Δt – sampling time interval in read-out direction

τ_{pe} – duration of the phase-encode gradient blip

ΔG_{yo} – phase-encode gradient peak

$$\begin{aligned}
 T_D &= N_y(T_s + \Delta T) \\
 &= N_x N_y \Delta t + N_y \Delta T
 \end{aligned}$$

$$T_T = \tau_{rf}/2 + t_0 + T_D$$

$$T_{E, \vec{k}=0} = \frac{N_y + 1}{2} N_x \Delta t + (N_y + 1) \tau_{rt} + t_0$$

Setting the Imaging Parameters

$L_x, G_x, \Delta x, N_x$

$L_y, \Delta G_y, \Delta x, N_y$

You could fix G_x to $G_{x,max}$ to minimize scan time and T_2^* filtering effects.

Setting the Imaging Parameters

$L_x, G_x, \Delta x, N_x$
 $L_y, \Delta G_{y0}, \Delta x, N_y$

You could fix G_x to $G_{x,max}$ to minimize scan time and T_2^* filtering effects.

$$\Delta t = \frac{1}{\gamma G_x L_x} \quad N_x = \frac{L_x}{\Delta x}$$

$$\int_t^{t+\tau_{pe}} dt' \Delta G_y(t') = \frac{1}{\gamma L_y}$$

$$\Delta G_{y0} = 2/(\gamma L_y \tau_{pe})$$

$$\tau_{pe} = 2\tau_{rt}$$

$$\Delta G_{y0} = 1/(\gamma L_y \tau_{rt})$$

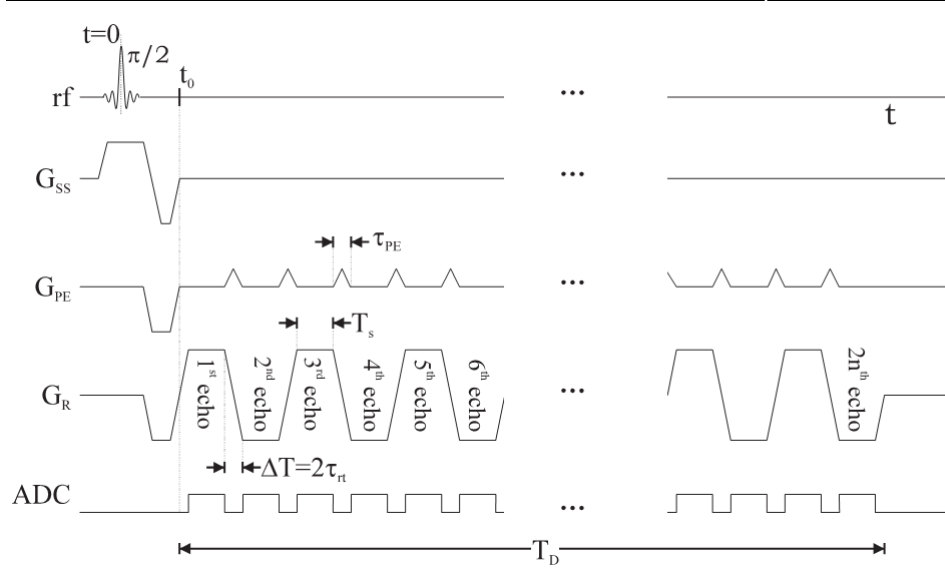
of PE lines that could be sampled is determined by a few parameters:

T_2^* filtering effects, Signal available and maximum gradient strength or sampling time for a given read-out.

$$N_{y,max} \simeq \frac{T_2^*}{N_x \Delta t + 2\tau_{rt}}$$

$$\Delta y_{min} \simeq \frac{L_y}{N_{y,max}}$$

Effect of Chemical-shift (Distortion) in phase encoding direction in EPI (Rectilinear sampling)



Δt is DW

$$\Delta\phi_r = 2\pi\gamma[G_r x DW + \Delta B_0(x, y, z)DW],$$

Conventional GRE

$$\Delta\phi_{pe} = 2\pi\gamma\Delta G_{pe} y \tau_{pe}$$

EPI - GRE

$$\Delta\phi_r = 2\pi\gamma[G_r x DW + \Delta B_0(x, y, z)DW],$$

[4]

$$\Delta\phi_{pe} = 2\pi\gamma[G_{pe} y \tau_{ramp} + \Delta B_0(x, y, z)(2\tau_{ramp} + N.DW)]$$

Effect of Chemical-shift (Distortion) in phase encoding direction in EPI (Rectilinear sampling)

$$\phi_{\sigma}(k_x, (p+1)\Delta k_y) - \phi_{\sigma}(k_x, p\Delta k_y) = \gamma \Delta B_{\sigma} \Delta \tau_{pe}$$

$$\Delta \tau_{pe} \equiv T_s + 2\tau_{rt}$$

$$\begin{aligned} n_{\sigma,pe} &= \frac{N_y(\phi_{\sigma}(k_x, (p+1)\Delta k_y) - \phi_{\sigma}(k_x, p\Delta k_y))}{2\pi} \\ &= N_y \gamma \Delta B_{\sigma} \Delta \tau_{pe} \end{aligned}$$

Along **Read** direction...

$$n_{\sigma,r} = N_x \gamma \Delta B_{\sigma} \Delta t$$

Comparing both...

$$\frac{n_{\sigma,pe}}{n_{\sigma,r}} = \frac{N_y}{N_x} \cdot \frac{\Delta \tau_{pe}}{\Delta t}$$

Ch22 - Quantifying Basic Tissue Properties of Spindensity, T1 and T2

$$M_0 \simeq \rho_0 \frac{s(s+1)\gamma^2 \hbar^2}{3kT} B_0 \quad (\hbar\omega_0 \ll kT)$$

$$\hat{\rho}(T_R, T_E) = \rho_0 e^{-T_E/T_2} (1 - e^{-T_R/T_1}) \quad T_R \gg T_E$$

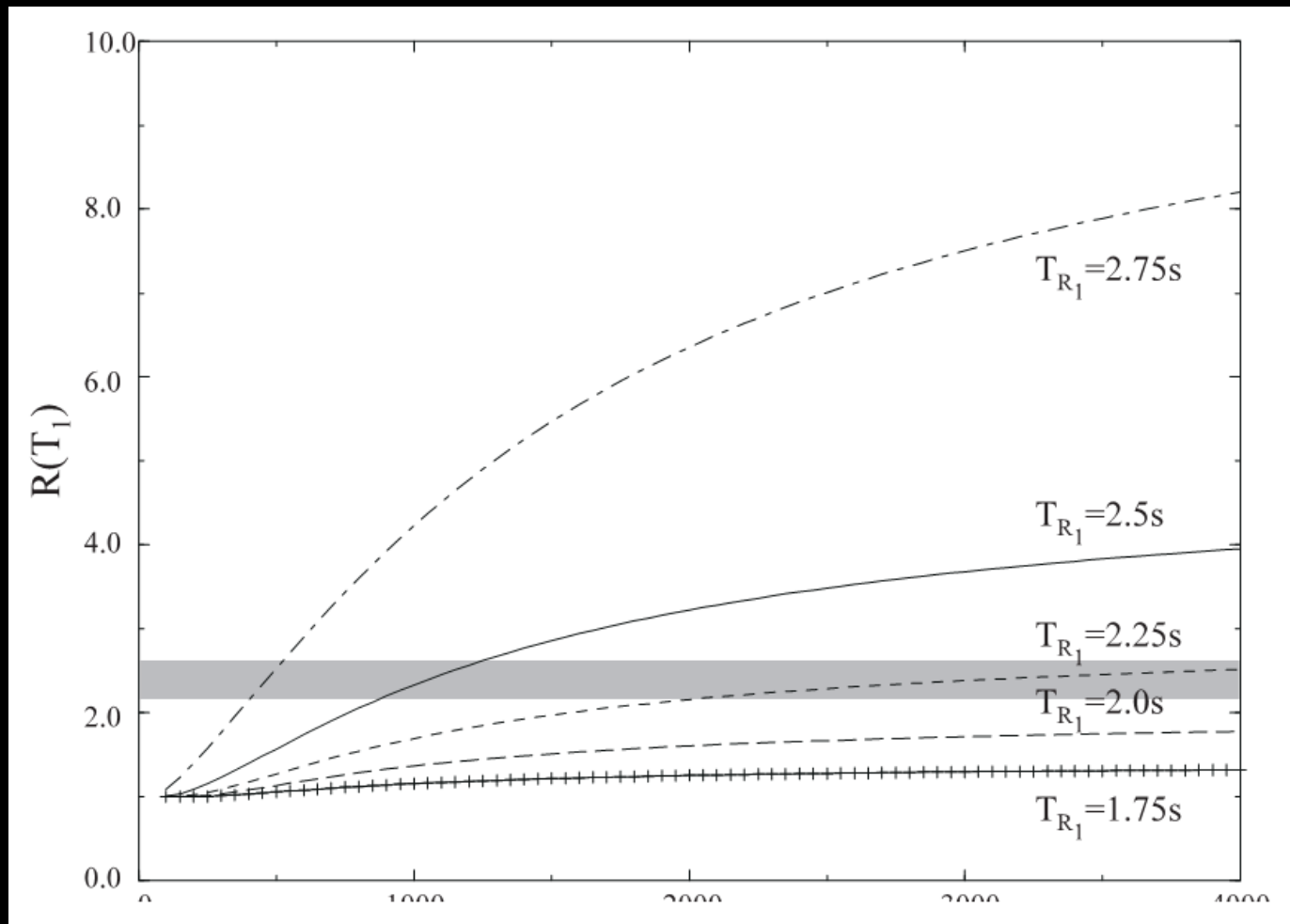
$$T_E \simeq T_2$$

$$T_E \ll T_2$$

$$T_R \gg T_1$$

$$T_R \ll T_1$$

$$R \equiv \frac{\rho_1}{\rho_2} = \frac{(1 - e^{-T_{R_1}/T_1})}{(1 - e^{-T_{R_2}/T_1})}$$



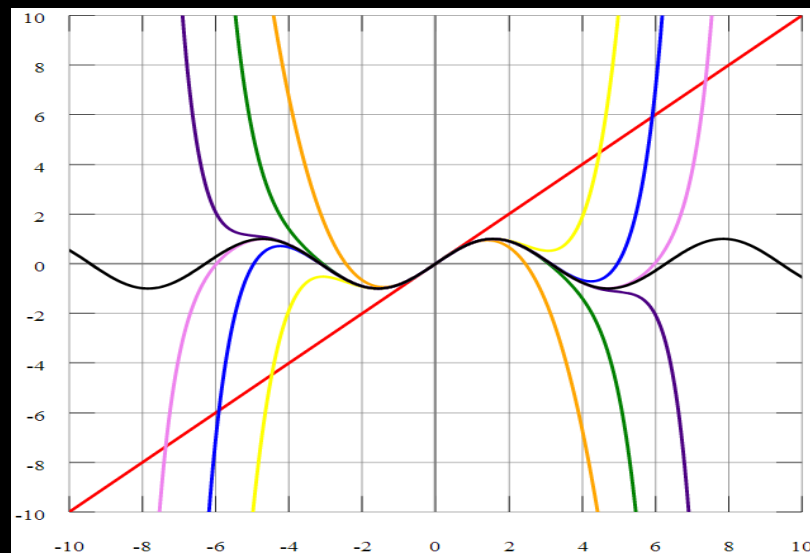
Ch22 – Error Propagation

Taylor Expansion

$$X = f(u, v)$$

If we have a small error in the independent variables u or v that we are essentially measuring, then what is the resultant error in the dependent variable X that we are attempting to quantify

$$f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \frac{f^{(3)}(a)}{3!}(x-a)^3 + \dots$$



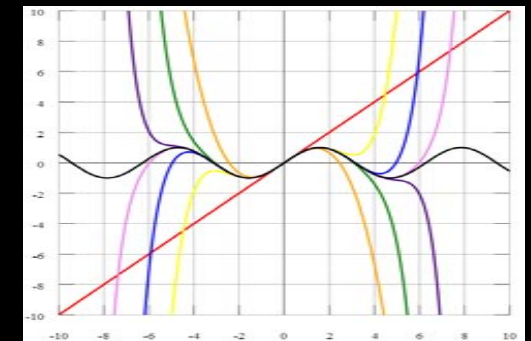
As the degree of the Taylor polynomial rises, it approaches the correct function.
This image shows and Taylor **Sin(x)** approximations, polynomials of degree 1, 3, 5, 7, 9, 11 and 13.

Ch22 – Error Propagation Taylor Expansion

Essentially Taylor Series expansion of a function to the first order, around a particular value of the independent variable, computes the linear approximation of the function around that value.

1D function

$$f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \frac{f^{(3)}(a)}{3!}(x-a)^3 + \dots$$



$F(x)$ = some differentiable
function in x

So, if we deviate from 'a' by a small amount, what will the value of $f(x)$ be can be obtained in the first order (as long as $(x-a)$ is really small), from the first order term of the Taylor series expansion of $f(x)$.

2 D function

$$f(x, y) \approx f(a, b) + (x-a) f_x(a, b) + (y-b) f_y(a, b) + \frac{1}{2!} [(x-a)^2 f_{xx}(a, b) + 2(x-a)(y-b) f_{xy}(a, b) + (y-b)^2 f_{yy}(a, b)] ,$$

Ch22 – Error Propagation Taylor Expansion

Example

$$V_0 = L_0 W_0 H_0$$

Ignoring the higher order terms

$$V \simeq V_0 + \Delta L \left(\frac{\partial V}{\partial L} \right)_{W_0 H_0} + \Delta W \left(\frac{\partial V}{\partial W} \right)_{L_0 H_0} + \Delta H \left(\frac{\partial V}{\partial H} \right)_{L_0 W_0}$$

Generalization

$$x = f(u, v, \dots)$$

$$\sigma_x^2 \simeq \sigma_u^2 \left(\frac{\partial x}{\partial u} \right)^2 + \sigma_v^2 \left(\frac{\partial x}{\partial v} \right)^2 + \dots + 2\sigma_{uv}^2 \left(\frac{\partial x}{\partial u} \right) \left(\frac{\partial x}{\partial v} \right) + \dots$$

If noise in u and v are uncorrelated then σ_{uv}^2 is 0, so

$$\sigma_x^2 \simeq \sigma_u^2 \left(\frac{\partial x}{\partial u} \right)^2 + \sigma_v^2 \left(\frac{\partial x}{\partial v} \right)^2 + \dots$$

$$\hat{R} \equiv \frac{\hat{\rho}_1}{\hat{\rho}_2} \simeq R \left(1 + \frac{\epsilon_1}{\rho_1} - \frac{\epsilon_2}{\rho_2} \right)$$

$$\frac{\sigma_{\hat{R}}^2}{R^2} = \sigma^2 \left(\frac{1}{\rho_1^2} + \frac{1}{\rho_2^2} \right) = \frac{1}{\text{SNR}_1^2} (1 + R^2)$$

$$\begin{aligned}\rho_1 &= \rho_0 e^{-T_{E_1}/T_2} (1 - e^{-T_R/T_1}) \\ \rho_2 &= \rho_0 e^{-T_{E_2}/T_2} (1 - e^{-T_R/T_1})\end{aligned}$$

$$\hat{T}_2 = \frac{(T_{E_2} - T_{E_1})}{\ln\left(\frac{\rho_1}{\rho_2}\right)}$$

$$\frac{\sigma_{\hat{T}_2}}{T_2} = \frac{\sigma}{\rho_0} \cdot \frac{T_2}{(T_{E_2} - T_{E_1})} \cdot \left[\frac{\sqrt{(e^{-2T_{E_1}/T_2} + e^{-2T_{E_2}/T_2})}}{e^{-(T_{E_1} + T_{E_2})/T_2}} \right]$$

$$\hat{\rho}_{\text{ssi}}(\theta) = \rho_0 e^{-T_E/T_2^*} \frac{(1 - E_1) \sin \theta}{(1 - E_1 \cos \theta)}$$

$$\frac{\hat{\rho}_{\text{ssi}}(\theta)}{\sin \theta} = E_1 \frac{\hat{\rho}_{\text{ssi}}(\theta)}{\tan \theta} + \rho_0 e^{-T_E/T_2^*} (1 - E_1)$$

